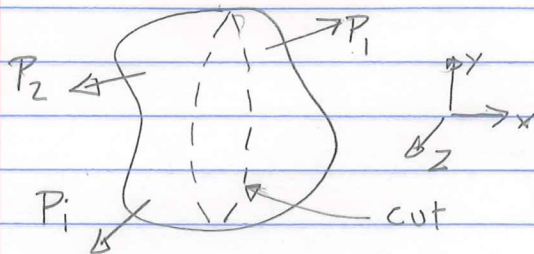
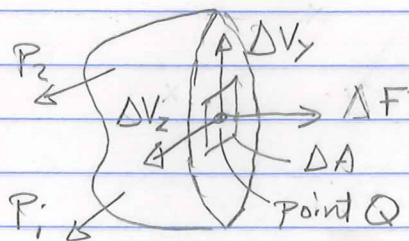


1. Stress definition

Consider a body loaded with forces



Cut the body along a plane parallel to y - z . Examine the part of the body to the left of the cut with a FBD.



x is $\perp$ to plane of cut; y, z are parallel. ΔF , ΔV_y and ΔV_z are the x, y, z components of the resultant force on the small area ΔA . (ΔF is a normal component, and ΔV_y and ΔV_z are shear components.)

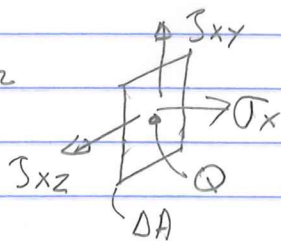
Shrink the area ΔA around point Q .

Define the $\lim_{\Delta A \rightarrow 0} \frac{\Delta F}{\Delta A}$ as the normal stress σ_x at point Q .
axis $\perp$ to ΔA

Define the $\lim_{\Delta A \rightarrow 0} \frac{\Delta V_y}{\Delta A}$ as the shear stress τ_{xy} at point Q .
axis $\perp$ to ΔA component of shear stress

Define the $\lim_{\Delta A \rightarrow 0} \frac{\Delta V_z}{\Delta A}$ as the shear stress τ_{xz} at point Q .
axis $\perp$ to ΔA component of shear stress

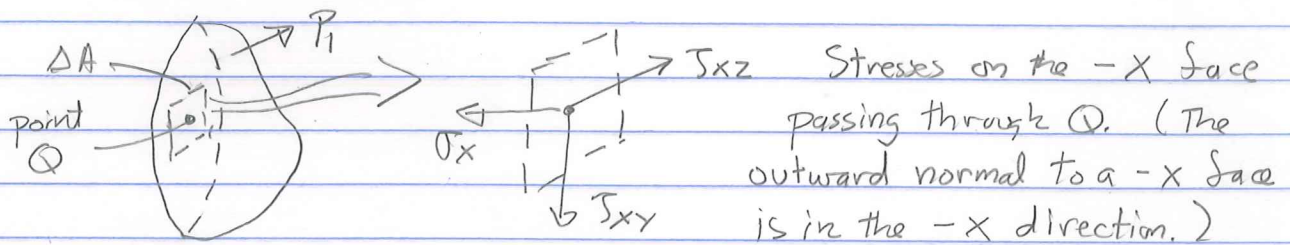
The above stresses can be depicted as:



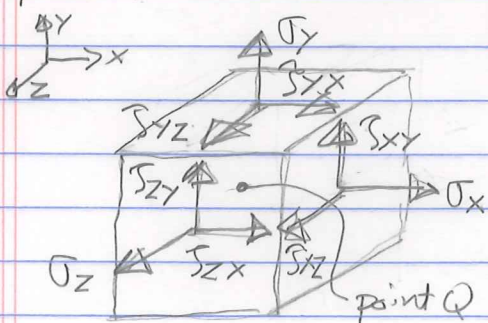
These are stresses on the $+x$ face passing through Q . (The outward normal to a $+x$ face is in the $+x$ direction.)

Stress is a vector and the quantities $\sigma_x, \tau_{xy}, \tau_{xz}$ are the x, y, z components of the stress vector acting on ΔA . The arrows show the direction of the components, but the stresses are actually distributed over ΔA . As $\Delta A \rightarrow 0$, the distribution of stress approaches being uniform, which are the stresses at point Q .

If we had considered the right-side free body, the same stresses would have been obtained at Q, but in opposite directions.



Repeating the above limiting process on a small cube around point Q reveals additional stress components:

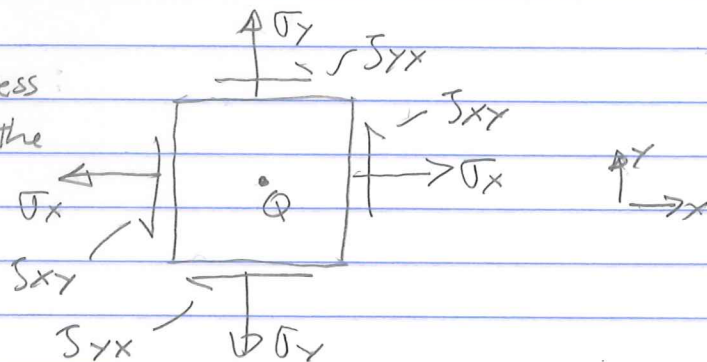


Only the stress components on the $+x, +y, +z$ faces are shown; ones on the $-x, -y, -z$ faces (hidden) are not shown.

Sign convention: positive stresses are in the $+x, +y, +z$ directions on $+$ faces, and in the $-x, -y, -z$ directions on $-$ faces. For the τ stresses, the first subscript denotes the face and the second denotes the component.

For a 2-d state of stress (plane stress), say, for the $x-y$ plane:

All stresses are shown according to the positive sign convention.



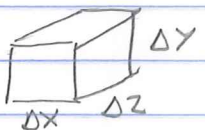
As indicated, the 3-d state of stress at a point can be expressed with respect to x, y, z by 9 components (3 normal, 6 shear). However, this description can be reduced to 3 normal and 3 shear as follows:

$\sum \bar{M} = 0$ about any axis for static equilibrium.

$$\sum M_y = \tau_{xy} \cdot \Delta y \Delta z \cdot \Delta x - \tau_{yx} \cdot \Delta x \Delta z \cdot \Delta y$$

$$= 0 \Rightarrow \tau_{xy} = \tau_{yx}, \text{ where it is assumed}$$

that $\Delta x, \Delta y, \Delta z$ are small enough so that the stresses can



be assumed to be uniform.

Similarly, $\sum M_x = 0 \Rightarrow \tau_{yz} = \tau_{zy}$

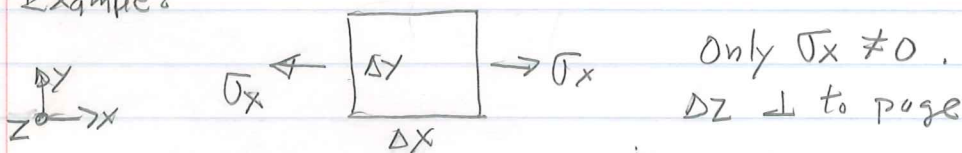
and $\sum M_y = 0 \Rightarrow \tau_{xz} = \tau_{zx}$

The x, y, z stress state is usually referred to as $\sigma_x, \sigma_y, \sigma_z, \tau_{xy}, \tau_{xz}, \tau_{yz}$. (3 normal, 3 shear)

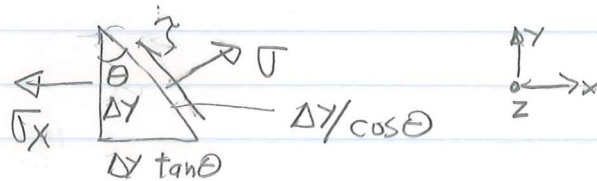
For plane stress, say in the $x-y$ plane, the x, y stress state is $\sigma_x, \sigma_y, \tau_{xy}$ (2 normal, 1 shear).

The x, y, z stress state is sufficient to determine the stress components at a point on any plane at any orientation.

Example:



Want to find σ, τ



$$\sum F_x = 0 : -\sigma_x \cdot \Delta y \Delta z + \sigma \cos \theta \frac{\Delta y}{\cos \theta} \Delta z - \tau \sin \theta \frac{\Delta y}{\cos \theta} \Delta z = 0$$

$$\sum F_y = 0 : \tau \sin \theta \frac{\Delta y}{\cos \theta} \Delta z + \tau \cos \theta \frac{\Delta y}{\cos \theta} \Delta z = 0$$

$$\text{Solve: } \sigma = \sigma_x \cos^2 \theta ; \tau = -\sigma_x \cos \theta \sin \theta$$

All of the above concepts of stress apply equally well to dynamic problems.